

Piezoelectric transducer design for electric power generation

Diseño de transductor piezoeléctrico para generación de potencia eléctrica

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Abstract

Working on alternatives for harnessing and transforming different forms of energy in a clean and efficient way, like piezoelectric phenomena, allows to consider collecting energy that is commonly wasted. For example, the piezoelectricity facilitates the harvesting of energy derived from the weight discharged by humans when walking on a surface conditioned with piezoelectric transducers. However, the technology in this field has always advanced in the opposite direction, i.e. conversion of electric energy into vibrations for different applications. In this work, the design of the material structure for a piezoelectric device of low resonance frequency for the capture of electricity is considered. The purpose of this device is the efficient transformation of mechanical energy into electrical energy, for this reason the design of its configuration considers a resonance frequency of less than 100 kHz. For this, the characteristics of the area dimensions and their relationship to the thickness according to the deposited material and the performance according to the projected impact were established. In addition, the selection of the substrate was considered according to the fracture requirements, considering the mechanical loading loads of the transducer.

Keywords: energy; frequency; piezoelectric; transducer; transformation.

Resumen

Al trabajar en alternativas para aprovechar y transformar diferentes formas de energía de una manera limpia y eficiente, se considera el fenómeno piezoeléctrico, el cual permite la recolección de energía que comúnmente se desperdicia. Por ejemplo, la piezoelectricidad facilita la recolección de energía derivada del peso descargado por los humanos cuando se camina sobre una superficie acondicionada con transductores piezoeléctricos. Sin embargo, la tecnología en este campo siempre ha avanzado en la dirección opuesta, es decir, la conversión de energía eléctrica en vibraciones para diferentes aplicaciones. En este trabajo, se considera el diseño de la estructura del material para un dispositivo piezoeléctrico de baja frecuencia de resonancia para la captura de electricidad. El propósito de este dispositivo es la transformación eficiente de la energía mecánica en energía eléctrica, por esta razón el diseño de su configuración considera una frecuencia de resonancia de menos de 100 kHz. Para esto, se establecieron las características de las dimensiones del área y su relación con el espesor de acuerdo con el material depositado y el rendimiento de acuerdo con el impacto proyectado. Además, la selección del sustrato se consideró de acuerdo con los requisitos de fractura, teniendo en cuenta la magnitud de carga mecánica al transductor.

Palabras clave: piezoeléctrico; energía; frecuencia; transformación, transductor.

1. Introduction

The need to find transformation alternatives capable of taking advantage of daily human activities, orient the look to the piezoelectric phenomenon, this propriety of some materials to transform mechanical movements into electricity, for example, it can be exploited while walking. For this you can arrange the piezoelectric transducer in shoes or directly on the floor. The contribution of this work allows to obtain experience in the own design of devices and materials that performance the energy conversion.

Nowadays, the technology has advanced in the development of different transducers, where its manufacture and performance are subject to the characteristics of the materials used in the process. Different piezoelectric elements manufactured that are used as transforming elements of mechanical energy into electrical energy, however, the designs found have characteristics for specific applications and are commercially expensive. In this paper we present a study of the different possibilities that have been taking care of the piezoelectric characteristics such as voltage, power and frequency for electricity generation.

Moreover, this paper discusses the effect of geometric parameters in obtaining different characteristics for an efficient transformation of mechanical energy into electrical energy, so that the design of the piezoelectric configuration considers a resonance frequency of less than 100 kHz

2. Physical principle

A piezoelectric crystal can be defined as a crystal in which electricity or electric polarity is produced by pressure, or is electrified to compression. Reciprocally it is defined as a material with an electric field.

When a piezoelectric material is subjected to a compression or a positive pressure this acquires polarity. If the pressure is replaced by a stretching (i.e. a change of sign of pressure) the sign of the electric polarity is reversed, too. Then the piezoelectric effect is the electrical response that a material has against a positive or negative value of mechanical pressure applied between its ends. A crystal structure with piezoelectric properties has defined some parameters to quantify its response. An important parameter is the "one - wayness" or region where the sign of the pressure exerted is determined. In the opposite effect, the same one- wayness determines the sign of deformation when an electric field is applied to the crystal. This change of sign gives the

voltage with the field sample that distinguishes the electrostriction piezoelectricity.

A pressure exerted on two piezoelectric crystals causes a deformation of its molecular state causing a collision between atoms. When the crystal is compressed, the ionized (charged) atoms present in the structure of each cell of formation of the crystal move, causing the electric polarization of it. Due to the regularity of the crystal structure, and as the deformation effects of the cell occur in all the cells of the body of the crystal, these charges add up and an accumulation of the electric charge occurs, producing a difference of electric potential between certain Faces of the crystal in which the pressure is exerted.

Of the 32 crystals classes, there are 20 that possess one - wayness [1]. In the others, there is no way to determine the direction of compression or polarity, as these materials are not significantly polarized.

The effect of applying a voltage to deform a crystal is not always reciprocal, it depends on the structure of the crystal because the deformation can be pure or at different angles with respect to the electric field.

A piezoelectric crystal is one that deforms in an electric field, depending on the relationship between the applied voltage and the resulting polarization. Stress can be a compression or an extension, but it can also be a shear stress, which is closely related to compression. There is a kind of crystal in which a random stress produces a polarization, proportional to the direction and amount of it, of course, vary with stress. This material is called triclinic asymmetric and corresponds to the material of lower symmetry at present. There are no materials with piezoelectric properties in a single direction, but there are several kinds of materials where polarization is limited in one plane [1]. In contrast, an applied field must have at least one component in the order of the plane where piezoelectric deformation occurs.

3. Discussion

The most relevant parameters in the study of piezoelectric materials, are the piezoelectric coupling factor K (K_{33} , K_{31} , K_P and K_t), mechanical quality factor (Q_m), frequency constant (NI), and piezoelectric coefficients of voltage (g_{33} and g_{31}) and displacement per charge (d_{33} and d_{31}) [1].

At present different materials are found with piezoelectric characteristics, however the application leads to choose materials with specific properties, for electric power generation, the ceramic materials of

excellent properties are PZT (5 A, 5H), PMN-PT, ZnO used as bulk material [2, 3].

Table 1. Piezoelectric Properties [2].

Property	Units	Symbol	PZT 5 A	PZT 5H	PMN-PT	ZnO
Density	$\frac{g}{cm^3}$	P	7,8	7,8	8,0	5,6
Dielectric Constant (< 100 KHz)	-	K^T_3	1900	3800	5400	87,0
Mechanical Quality Factor	-	Q_m	80	30	80	120
Coupling Coefficients	-	k_p	0,65	0,75		0,33
		k_{33}	0,72	0,75	0,91	0,42
		k_{31}	0,36	0,43	0,44	-
		k_t	0,48	0,55	0,60	0,46
Piezoelectric Charge (Displacement) Coefficient	$\frac{C}{N} \times 10^{-12}$ or $\frac{m}{V} \times 10^{-12}$	d_{31}	-190	-320	-699	-5,4
		d_{33}	390	650	1540	11,7
Piezoelectric Voltage Coefficient	$\frac{V \cdot m}{N} \times 10^{-3}$	g_{33}	24,0	19,0	32,2	15,2
		g_{31}	-11,3	-9,5	-14,6	-7,0
Elastic Modulus	$\frac{N}{m^2} \times 10^{10}$	Y^E_{11}	6,7	6,3	1,9	20,97
		Y^E_{33}	5,3	5,0	1,7	21,09
Poisson's Ratio	-	Y	0,31	0,31	0,37	0,31
Acoustic velocity	m/s	V_s	4350	4560	1540	2724

3.1. Frequency of resonance according to geometry of the piezoelectric material

The resonance frequency is determined by the parameters of the piezoelectric material as well as the determination of its geometric structure [1, 4]. According to the purpose of this work, it is important to determine and guide the

design at low frequencies, because the mechanical impacts considered are also of low frequencies.

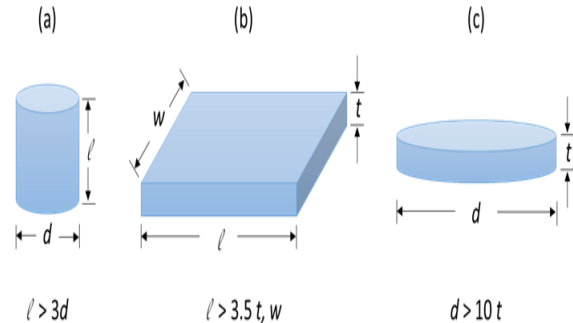


Figure 1. Design features of different geometries of piezoelectric material. (a) Pole rod, and (b) thin flat plate and (c) thin flat disc.

The resonance frequency for different geometries of piezoelectric material is determined by equations 1 y 2.

$$N_l = l * f_r = \frac{1}{2} \sqrt{\frac{Y}{\rho}} \quad (1)$$

$$f_r = \frac{V_s}{2 * t} \quad (2)$$

Where l is the length of piezoelectric ceramic thin plate, t is the thickness of thin flat disc, V_s the sound velocity, f_r is the resonance frequency in the length direction, Y is the Young's modulus, and ρ is the density [1, 2].

Table 2. Resonance frequency

	Geometry	Pole rod	Thin flat plate	Thin flat disc
	Dimensions	l (30), d (10) mm	t (10), $l = w$ (35) mm	t (10), d (100) mm
f_r (kHz)	PZT 5 A	72.5	37.23	217,5
	PZT 5H	76.0	36.17	228
	PMN-PT	25.7	225.87	77
	ZnO	45.4	87.67	136,2

3.2. Capacitance according to geometry of the piezoelectric material

The capacitance for different geometries of piezoelectric material is determined by equations 3 y 4 [5].

$$C_p = \frac{l \cdot W \cdot k_3^T}{4.45 \cdot t} \quad (3)$$

$$C_d = \frac{d^2 \cdot k_3^T}{5.67 \cdot t} \quad (4)$$

Where Cp and Cd are the thin flat plate and thin flat disc capacitance respectively, l, W, d (in) and t (10⁻³ in) [3].

Table 3. Capacitance

	Geometry	Pole rod	Thin flat plate	Thin flat disc
	Dimensions	l (30), d (10) mm	t (10), l = w (35) mm	t (10), d (100) mm
C (nF)	PZT 5 A	43.98	2059.19	13192.79
	PZT 5H	87.95	4118.38	26385.59
	PMN-PT	124.98	5852.43	37495.31
	ZnO	2.01	94.29	604.09

3.3. Voltage generated by applied load according to geometry of the piezoelectric material

The piezoelectric constant dij is the ratio of short circuit charge per unit area flowing between connected electrodes perpendicular to the j direction to the stress applied in the i direction. As shown in Figure 2, once a force F is applied to the transducer, in the 3 direction, it generates the stress [6].

One of the considerations of the simulation is the ability to withstand mechanical stress according to the geometric structure as seen in figures 3, 4, and 5, for each of the geometries used. That is why it is considered a detailed analysis of the power generation capacity, taking into consideration the applied force.

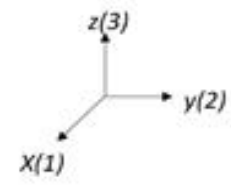
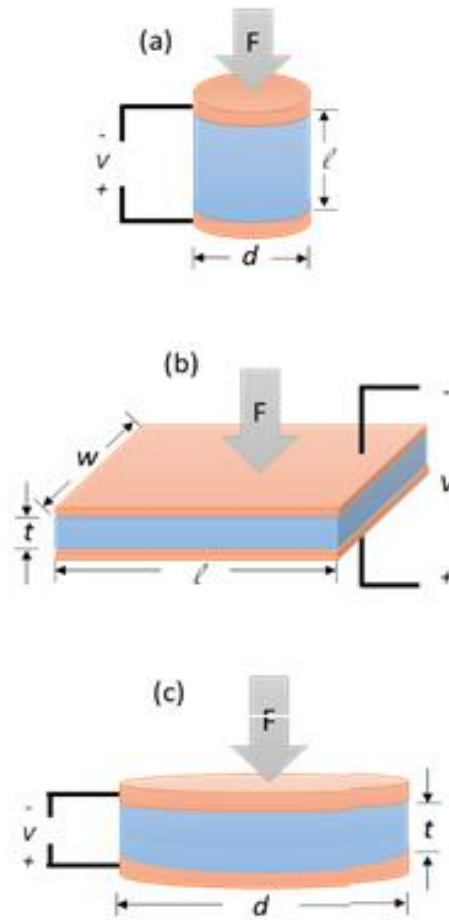


Figure 2. Voltage generated by applied load according geometries of piezoelectric material. (a) Pole rod, and (b) thin flat plate and (c) thin flat disc.

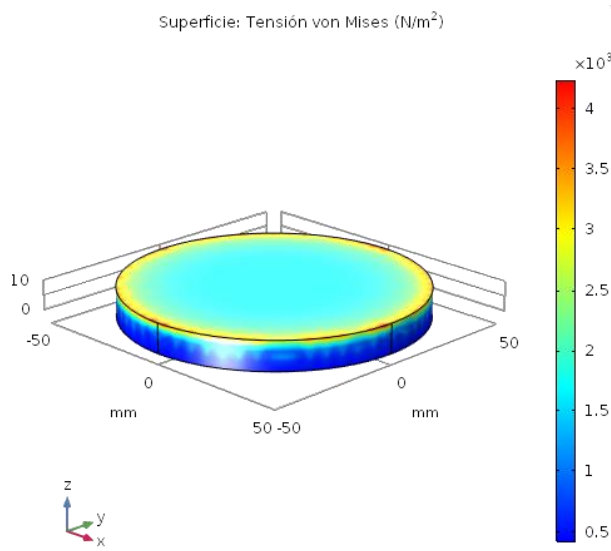


Figure 3. Applied load according geometries of piezoelectric material - thin flat disc.

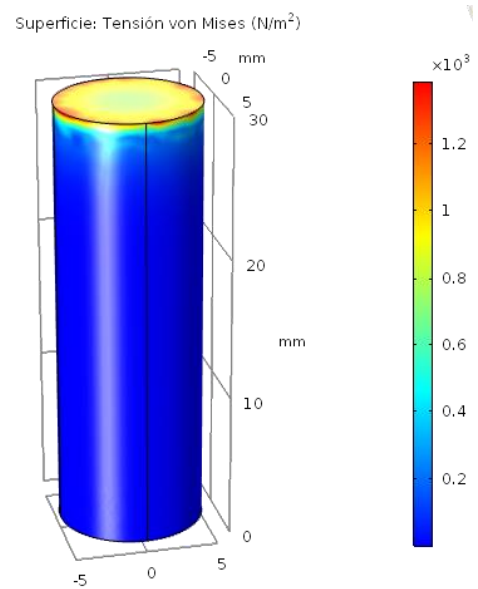


Figure 5. Applied load according geometries of piezoelectric material – pole rod.

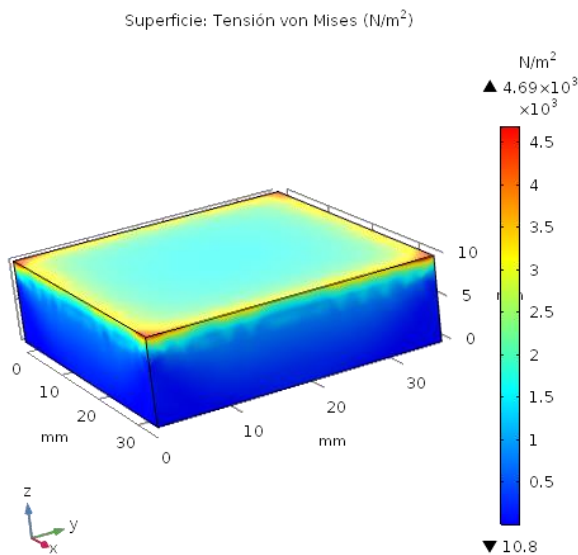


Figure 4. Applied load according geometries of piezoelectric material - flat plate.

The voltage generated by applied load for different geometries of piezoelectric material is determined by equations 3 y 4.

$$q = d_{33}F \quad (5)$$

$$V_p = \frac{g_{31}F}{C_p} \quad (6)$$

From the distribution of the force applied to the piezoelectric material as a function of the geometries studied, the electric voltage generated by the action of an external force is obtained, resulting in the figures 6, 7 and 8.

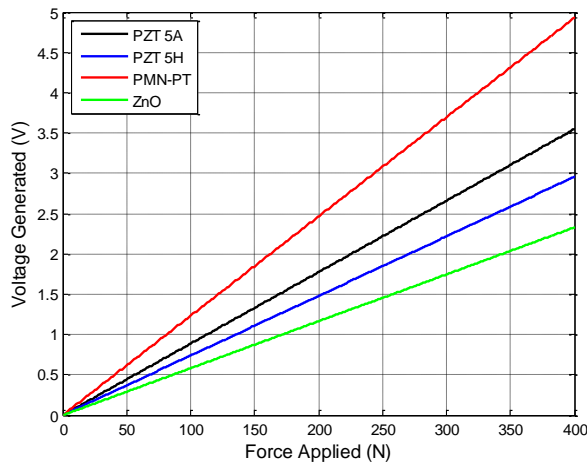


Figure 6. Voltage generated by applied load according geometries of piezoelectric material - Pole rod.

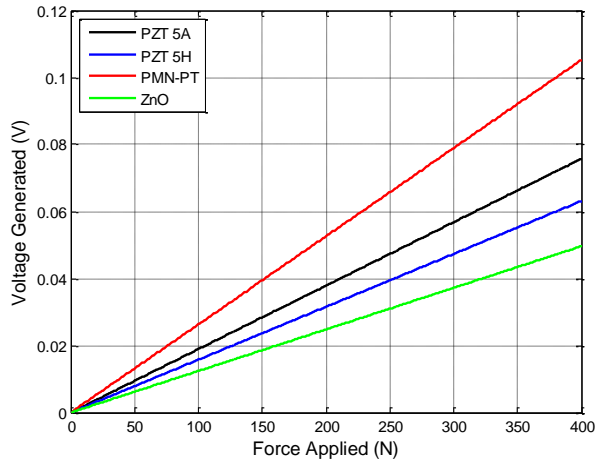


Figure 7. Voltage generated by applied load according geometries of piezoelectric material - thin flat plate.

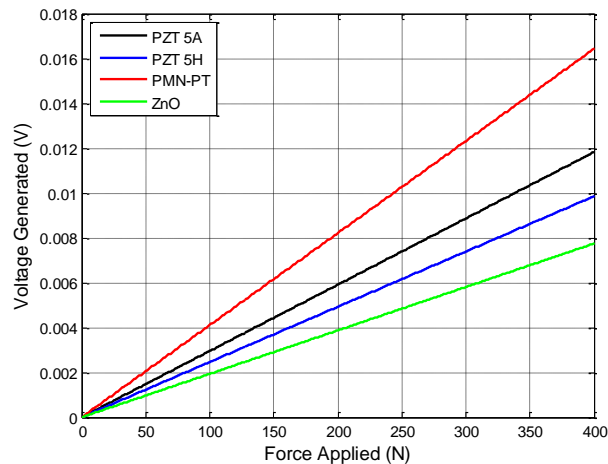


Figure 8. Voltage generated by applied load according geometries of piezoelectric material - thin flat disc.

From the figures 3, 4 and 5, it is possible to define the cylindrical geometric shape as a structure for the design of the transducer, considering that the possible generation of tension by applied force is greater in relation to its counterparts of thin planes. In addition to the above, it is important to note that the lowest frequencies that were obtained come from this structure.

4. Conclusions

In this paper is showed the justification for the design of a piezoelectric device with the purpose of obtaining electrical energy from mechanical impacts. For this, the foundation of the piezoelectric phenomenon and the parameters to consider for the design were presented. Moreover, different geometries were analyzed by simulation under the same conditions of effort, to select a definitive design.

As a result of this work, is presented the effect of geometric parameters in obtaining different characteristics for an efficient transformation of mechanical energy into electrical energy. It was found that the cylindrical geometry of the piezoelectric material favors the generation of greater electrical potential between the electrodes of the device, considering an increase of 99.53% with respect to the thin-plane geometry.

For the future works the material to be used is considered PMN-PT, given that its piezoelectric characteristics next to the design and geometry defined for the manufacture of the device, determined by this work.

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