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3 **COMPARISON OF THERMAL PERFORMANCES OF PLYWOOD SHEAR**  
4 **WALLS PRODUCED WITH DIFFERENT THERMAL INSULATION**  
5 **MATERIALS**

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18 **ABSTRACT**

19 Shear walls are one of the envelopes of light-frame wooden buildings where  
20 thermal insulation is most required. The thermal performance of shear walls can vary  
21 according to the type, properties and thickness of the wood and insulation materials used  
22 in their production. In this study, it was aimed to compare the thermal performances of  
23 plywood shear walls produced with different thermal insulation materials. For this aim,  
24 the archetype walls with properties similar to commonly used plywood shear walls were  
25 designed and produced for each thermal insulation material type and wood specie. The  
26 shear wall groups were formed by using Scots pine (*Pinus sylvestris*), black pine (*Pinus*  
27 *nigra*) and spruce (*Picea orientalis*) as wood species and cellulose, flax, felt, XPS, EPS,  
28 sheep's, rock and glass wool as thermal insulation materials. Thermal conductivity of the  
29 shear wall groups was determined according to the ASTM C518-04 standard. Thermal  
30 resistance and other thermal performance parameters were calculated using the thermal  
31 conductivity values. As a result of the study, rock wool was the best thermal insulation  
32 material among the Scots pine shear wall groups while glass wool was the best thermal  
33 insulation material among the black pine and spruce shear wall groups. The shear walls  
34 produced with EPS foam boards indicated the worst thermal performance among all  
35 groups

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38 **Keywords:** plywood, shear wall, thermal conductivity, thermal insulation materials,  
39 thermal performance.

## INTRODUCTION

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42 Building construction and operations caused 35 % of global total energy  
43 consumption and 38 % of energy-related CO<sub>2</sub> emissions in 2019 (United Nations  
44 Environment Programme 2020). In addition, it has been reported that the global energy  
45 consumption in buildings will grow by 1,3 % per year on average from 2018 to 2050 (IEA  
46 2020). These data indicate that energy efficiency and reduction of emissions are  
47 extremely important in the building industry. Building walls, which form a major part of  
48 the building envelope, interact thermally with the changing environment during the day  
49 (Jannat *et al.* 2020). Therefore, they are the building envelopes with the highest heat  
50 losses that cause the increase in energy consumption (Balaras *et al.* 2000). The thermal  
51 performance of the walls is an important factor in increasing the energy efficiency of the  
52 building industry and reducing greenhouse gas emissions. Thermal insulation is one of  
53 the most effective measures to increase energy efficiency by improving the thermal  
54 properties of building walls (Cetiner and Shea 2018). Energy savings up to 77 % can be  
55 achieved with the insulation of the wall and roof in the building (Çomaklı and Yüksel  
56 2003). Bio-based, petrochemical and mineral-based materials such as extruded  
57 polystyrene (XPS), expanded polystyrene (EPS), polyisocyanurate, polyurethane foam,  
58 cork, cotton, wood fibre, flax, hemp, coconut, cellulose, rice, sheep's wool, glass wool,  
59 rock wool can be used for thermal insulation in the building industry (Cetiner and Shea  
60 2018, Asdrubali *et al.* 2015).

61 Wooden structures can provide a better living environment compared to other  
62 building types with superior advantages such as environmentally friendly, energy  
63 efficiency, earthquake resistant, structural safety, health and comfort (Liu *et al.* 2018).  
64 Light-frame wood structures among the wood building types are widely preferred in low-

65 rise residences, commercial and industrial buildings, especially in Northern Europe and  
66 North America because of its similar advantages (Liu *et al.* 2021). They are  
67 conventionally formed of framing, sheathing materials, fasteners, and anchorage (Peng *et*  
68 *al.* 2020). Shear walls are the most important components affecting the structural and  
69 thermal performance of these structures. Thermal properties of the shear walls can be  
70 further improved by using suitable insulation materials besides the good thermal  
71 performance of sheathing materials. However, when choosing an insulation material, it is  
72 important to consider other important aspects such as acoustic performance,  
73 environmental impacts, impacts on human health and production costs (Asdrubali *et al.*  
74 2016, Schiavoni *et al.* 2016).

75 Thermal conductivity is a significant parameter used in both building and industrial  
76 processes in determining the heat transfer rate, developing drying models and adhesive  
77 curing rate (Hassanin *et al.* 2018, Kol and Altun 2009). In addition, when choosing  
78 insulation materials that are not affected by fluctuations in outdoor temperature and  
79 maintain indoor temperature, it is necessary to know the thermal conductivity values.  
80 Wood and wood-based materials give lower thermal conductivity values compared to  
81 other building materials due to their porous structure (Gu and Zink-Sharp 2005, Krüger  
82 and Adriazola 2010). The thermal conductivity of wood materials has varied according  
83 to wood species, wood fibre direction, resin type and additive members used in the  
84 manufacture of wood-based materials (Kamke and Zylkowski 1989, Hassanin *et al.*  
85 2018). Thermal conductivity values in the wooden shear walls can vary according to  
86 properties of the sheathing materials, wall thickness, space of frame and properties of the  
87 thermal insulation materials used in the cavities (Kosny *et al.* 2014).

88 The main purpose of this study is to compare the thermal performance of plywood  
89 shear walls produced with different thermal insulation materials. For this purpose, the  
90 archetype walls with properties similar to commonly used plywood shear walls were  
91 designed and produced for each thermal insulation material type and wood species.

## 92 MATERIALS AND METHODS

### 93 Materials and Manufacturing of Plywood

94 In this study, three species of coniferous wood, which are widely preferred in the  
95 building industry, were used: scots pine (*Pinus sylvestris*), black pine (*Pinus nigra*) and  
96 spruce (*Picea orientalis* L.). The logs for veneer manufacturing, with an average 40 cm,  
97 were obtained from Trabzon, located at the northern point of the Black Sea Region of  
98 Turkey. In addition, 40 mm thick cellulose, flax, felt, XPS, EPS, sheep's, rock and glass  
99 wool were commercially supplied as thermal insulation materials within the scope of the  
100 study. Cellulose, one of the insulation materials used in the study, was produced from 80  
101 percent recycled newsprint and 20 percent boric acid which was a non-toxic fire retardant.  
102 Flax was produced from recycled flax and hemp fibres whilst felt was produced from  
103 fibres obtained from the recycling of polyethylene terephthalate. Rock wool consisted of  
104 97% of natural fibres obtained from melting basalt stone while glass wool consisted of  
105 fibres produced by melting silica sand. Moreover, XPS boards was produced by extrusion  
106 of polystyrene raw material whilst EPS foams were produced by inflating polystyrene  
107 particles and sticking to each other and 98 % was composed of still dry air. Technical  
108 information about these thermal insulation materials was obtained from the suppliers.  
109 Furthermore, some technical specifications of these materials were given in Table 1.

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**Table 1:** Some Technical specifications of the thermal insulation materials.

<b>Thermal Insulation Material Types</b>	<b>Density (kg/m<sup>3</sup>)</b>	<b>Specific Heat Capacity (J/g °C)</b>	<b>Vapor Diffusion Resistance Factor</b>	<b>Thermal Conductivity (W/mK)</b>	<b>Measured* Thermal Conductivity at 30 °C (W/mK)</b>
Cellulose	40	1,4	2,1	0,040	0,042
Flax	36	1,6	2,4	0,040	0,043
Felt	70	1,3	1,9	0,040	0,040
Sheep's Wool	18	1,3	4,2	0,039	0,041
Rock Wool	45	0,9	1,2	0,033	0,038
Glass Wool	15	0,8	1,2	0,030	0,038
XPS	32	1,5	90	0,034	0,042
EPS	10	1,3	40	0,042	0,052

\* These were the values measured in the laboratory within the scope of the study. Other specifications were obtained from the suppliers.

113

In literature, the limit values of some specifications of building insulation materials

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were given in the study by Kumar *et al.* (2020). In this study, it was determined that some

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specifications values of the thermal insulation materials in Table 1 were in the range of

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these limit values. In addition, it was recalculated in the laboratory according to ASTM

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C518-04 (ASTM 2004) standard to compare the insulation materials more accurately

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within the scope of the study. Before the measurement, the thermal insulation materials

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were kept at 20 °C and 65 % relative humidity until they reached approximately 8 %

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moisture content.

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The logs were steamed for 12 hours - 16 hours at a temperature of 80 °C before the

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peeling process and veneer sheets with dimensions of 300 mm by 300 mm by 2 mm were

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clipped. The vertical opening was 0,5 mm and the horizontal opening was 85 % of the

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veneer thickness in the veneer manufacturing process. After rotary peeling, the veneers

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were dried at 110 °C in a veneer dryer until to reach 6 % - 7 % moisture content.

126 The Eurocode 8 states that the minimum thickness of the plywood boards to be used  
 127 in shear walls should be 9 mm (Bisch *et al.* 2012). Therefore, five-ply plywood panels,  
 128 10 mm thick, were manufactured by using phenol formaldehyde (PF) glue resin with 47  
 129 % solid content. The glue was applied at a rate of 160 g/m<sup>2</sup> to the single surface of veneer  
 130 by using a four-roller spreader. The assembled samples were pressed in a hot press at a  
 131 pressure of 0,785 MPa and at 140 °C for 10 min. The plywood panels were conditioned  
 132 to achieve equilibrium moisture content at 20 °C temperature and 65 % relative humidity  
 133 prior to testing.

134 Some physical specifications such as density, equilibrium moisture content (EMC)  
 135 and thermal conductivity values of plywood used in the shear walls and the veneers used  
 136 in plywood production were given in Table 2 according to tree species. The density, EMC  
 137 and thermal conductivity measurements were performed after drying in the veneers and  
 138 after conditioning in the plywood according to ISO 9427 (ISO 2003a), ISO 16979 (ISO  
 139 2003b) and ASTM C518 - 04 (ASTM 2004) standards, respectively.

140 **Table 2:** Some physical specifications of the veneers and plywood.

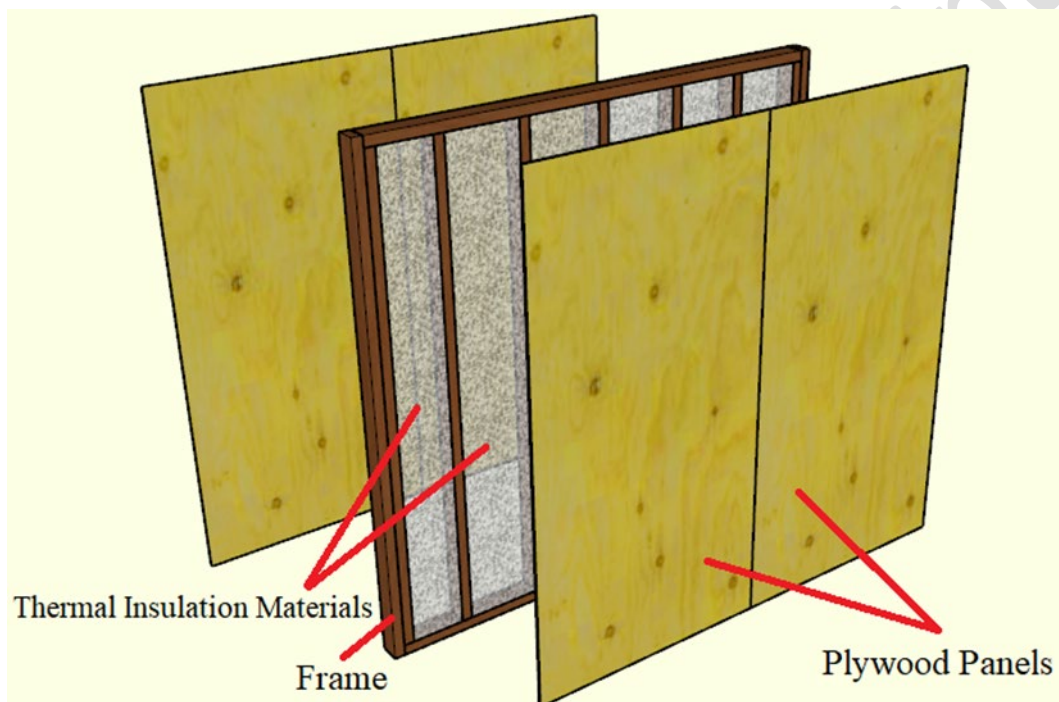
Material Type	Specifications	Wood Species		
		Scots Pine	Black Pine	Spruce
Veneer	Density (kg/m <sup>3</sup> )	498	523	462
	EMC (%)	6,21	6,28	6,17
	Thermal Conductivity (W/mK)	0,027	0,029	0,026
Plywood	Density (kg/m <sup>3</sup> )	587	596	512
	EMC (%)	8,42	8,64	8,21
	Thermal Conductivity (W/mK)	0,105	0,118	0,097

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143 **Manufacturing of Archetype Plywood Shear Wall**

144 The sheathed shear walls used in light-frame wooden structures are generally  
145 manufactured in the dimensions of 2,4 m x 2,4 m according to the dimensions given in  
146 ASTM E72 - 13a (ASTM 2014) Standard. In the building industry, the thermal properties  
147 of the shear walls are increased by filling the spaces between the frame and the sheathing  
148 materials with thermal insulation materials. Typical plywood shear walls and spaces  
149 where thermal insulation materials are used are shown in Figure 1.



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**Figure 1:** Typical plywood shear walls and use of thermal insulation materials.

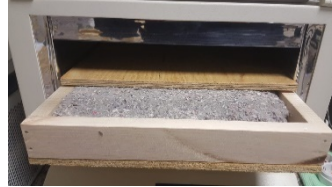


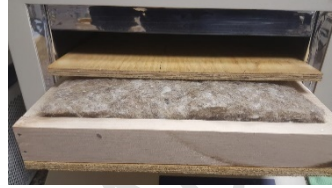



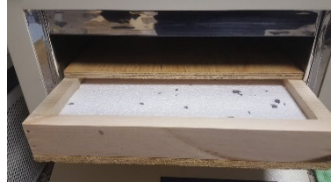
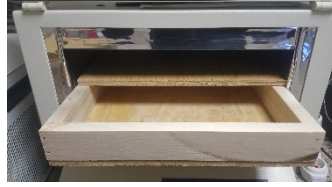
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152 Within the scope of the study, the archetype specimens of 300 mm x 300 mm were  
153 produced for each shear wall group formed according to the determined variables. They  
154 were used because both the specimen measurement dimensions of the test apparatus and  
155 the purpose of the study were to compare only the thermal insulation materials. The  
156 spruce timbers were used as frames in all the archetypal shear wall groups. The density  
157 of the timbers was 451 kg/m<sup>3</sup>, the moisture content was 12 % and the thermal conductivity

158 was 0,124 W/mK. The frame was produced with dimensions of 300 mm x 300 mm by  
 159 nailing from 4 pieces of spruce timber with a thickness of 40 mm and a width of 18 mm.  
 160 The control groups were formed to reveal the percentage differences of the thermal  
 161 conductivity coefficients of the thermal insulation materials from the shear walls  
 162 consisting of only the plywood panels and the frame filled with still air.

163 The descriptive information about the shear wall groups created to achieve the aim  
 164 of the study and the views of the test specimens are given in Table 3.

165 **Table 3:** The descriptive information and views of the archetype specimen groups.

Wood Species	Scots Pine	Black Pine	Spruce
Thermal Insulation Material Types			
	1. Cellulose	2. Flax	3. Felt
			
	4. Sheep's Wool	5. Rock Wool	6. Glass Wool
			
	7. XPS	8. EPS	9. Control

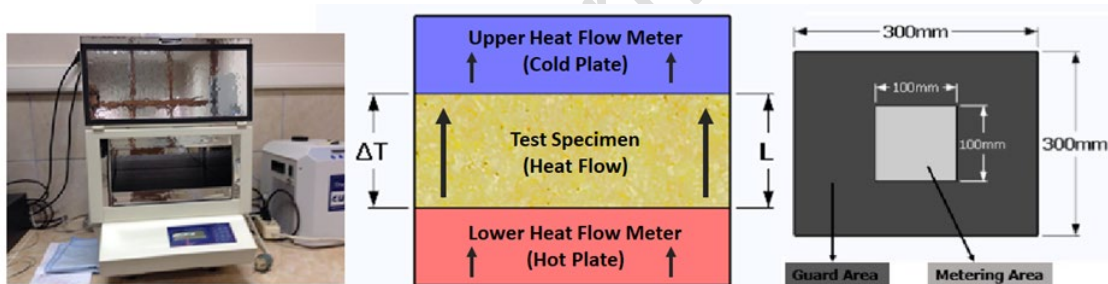
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167 **Thermal Performance Test**

168 The thermal conductivity, thermal resistance and other parameters that can be  
 169 calculated with these are considered as important measurements in the selection of  
 170 thermal insulation materials (Hassanin *et al.* 2018). In this study, the thermal conductivity



171 coefficients of archetype specimens were determined according to ASTM C518 - 04  
172 (ASTM 2004) at average 30 °C and FOX 314 Steady-State Heat Flow Meter apparatus  
173 (HFM) was used for these measurements (Figure 2). The thermal conductivity coefficient  
174 measurements were carried out with 6 repetitions for each group. Before the tests, the  
175 standard calibration of the HFM test machine was made and during the test, the 300 mm  
176 × 300 mm specimen was placed between the cold and hot plates. During the  
177 measurements, the temperature of the cold (upper) plate was set to 20 °C and the  
178 temperature of the hot (lower) plate to 40 °C. Moreover, all measurements were carried  
179 out in the laboratory at 20 °C and 65 % relative humidity. These plates have a guard area  
180 and a 100 mm x 100 mm dimensions metering area where the heat flow is measured  
181 (Figure 2).



182

183 **Figure 2:** Photo and schematic of the HFM apparatus.

184 The thickness of the test specimens was measured with four optical encoders, one  
185 on each corner of the plate, and the temperature drop across the specimen was measured  
186 with thermocouples placed on the plates. The temperature and voltage values were  
187 recorded for the upper and lower layers every 0,5 seconds, and these records were  
188 organized in groups of 512 called data blocks, one of which consists of approximately 4  
189 minutes of data. The software of the apparatus determined the average thermal  
190 conductivity with equation 1 by calculating the average temperatures and voltages of the  
191 plates for each data block. For the apparatus to measure the average thermal conductivity,

192 the last three data blocks must reach the steady state condition. This was achieved when  
193 the average temperature differences of the plates were within the limits of  $\pm 0,2$  °C and  
194 the average voltage value for a data block did not differ by more than 2 % of the previous  
195 data block.

$$196 \quad k = \frac{q'' \cdot L}{\Delta T} \quad (1)$$

197 where:

198 k: average thermal conductivity coefficient (W/mK)

199  $q''$ : heat flux (W/m<sup>2</sup>)

200  $\Delta T$ : temperature difference across the specimen (K)

201 Using equation 2, the percent differences of heat flow between the upper and lower  
202 plates of the device were determined.

$$203 \quad \% \text{Difference} = \frac{q''_U - q''_L}{q''} \quad (2)$$

204 Where:

205  $q''_U$ : upper heat flux (W/m<sup>2</sup>)

206  $q''_L$ : lower heat flux (W/m<sup>2</sup>)

207  $q''$ : average  $q''_U$  and  $q''_L$  (W/m<sup>2</sup>)

208 The capacity of a material to prevent heat flow in a certain area and under a certain  
209 temperature is called absolute thermal resistance (R) and the higher the absolute thermal  
210 resistance, the better the material's thermal insulation. R (absolute thermal resistance) and  
211 R-value, which is the thermal resistance of a material per unit area, were calculated with  
212 equations 3 and 4.

$$213 \quad R = \frac{L}{k \cdot A} \quad (3)$$

$$214 \quad \text{R-value} = \frac{L}{k} \quad (4)$$

215 where

216 R: absolute thermal resistance (K/W)

217 R-value: thermal resistance (m<sup>2</sup>K/W)

218 L: total thickness of the shear wall (m)

219 k: measured average thermal conductivity coefficient (W/mK)

220 A: metering area in (m<sup>2</sup>)

221 Moreover, thermal resistivity (r) and thermal conductance (C) values of the  
222 specimens in Km/W and W/m<sup>2</sup>K were calculated based on equations 5 and 6.

223 
$$r = \frac{1}{k} \quad (5)$$

224 
$$C = \frac{k}{L} \quad (6)$$

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## 226 **RESULTS AND DISCUSSION**

227 The thermal conductivity coefficient average values and percent differences of the  
228 shear wall groups formed within the scope of the study were given in Table 4 according  
229 to the wood species and thermal insulation material types. In addition, the thermal  
230 conductivity coefficient changes and percentage reduction in the thermal conductivity of  
231 these groups were graphically shown in Figure 3.

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**Table 4:** Thermal conductivity average values and percentage differences of the shear walls groups.

Wall Numbers	Wood Species	Thermal Insulation Material Types	Thickness (L-mm)	Thermal Conductivity (k-W/mK)	Percent Difference (%)
1	Scots Pine	Cellulose	59,11	0,059	12,58
2		Flax	59,30	0,059	3,32
3		Felt	59,17	0,057	2,06
4		Sheep's Wool	59,46	0,057	2,40
5		Rock Wool	59,25	0,055	1,46
6		Glass Wool	59,16	0,056	4,98
7		XPS	59,16	0,058	1,63
8		EPS	59,12	0,076	0,73
9		Control	59,10	0,200	5,05
10	Black Pine	Cellulose	60,60	0,059	3,44
11		Flax	60,67	0,061	2,67
12		Felt	60,62	0,058	2,13
13		Sheep's Wool	60,87	0,060	2,92
14		Rock Wool	60,69	0,057	2,33
15		Glass Wool	60,65	0,057	3,84
16		XPS	60,64	0,061	10,05
17		EPS	60,55	0,080	0,12
18		Control	60,61	0,213	6,55
19	Spruce	Cellulose	59,00	0,057	3,08
20		Flax	59,09	0,059	5,65
21		Felt	59,02	0,057	2,56
22		Sheep's Wool	59,23	0,058	2,72
23		Rock Wool	59,19	0,057	0,28
24		Glass Wool	59,00	0,056	1,61
25		XPS	59,01	0,057	0,37
26		EPS	58,94	0,075	0,27
27		Control	58,95	0,187	5,97

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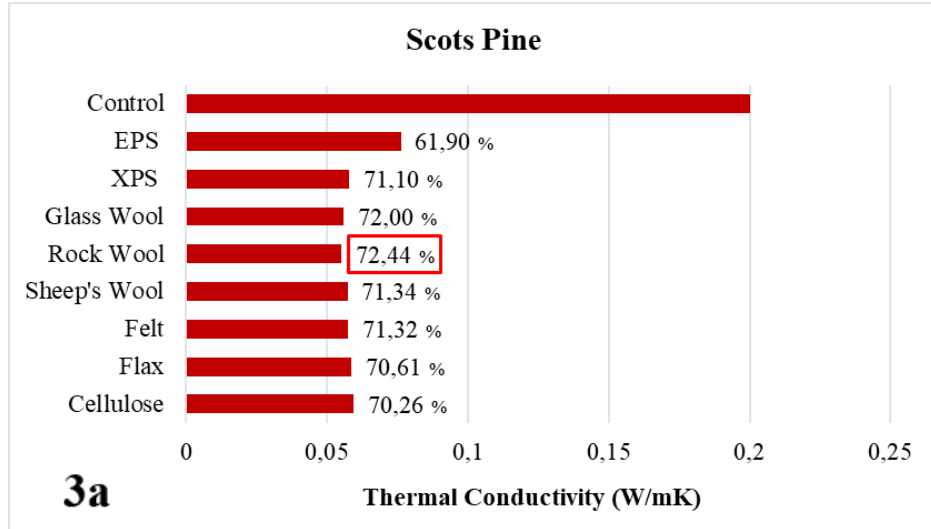
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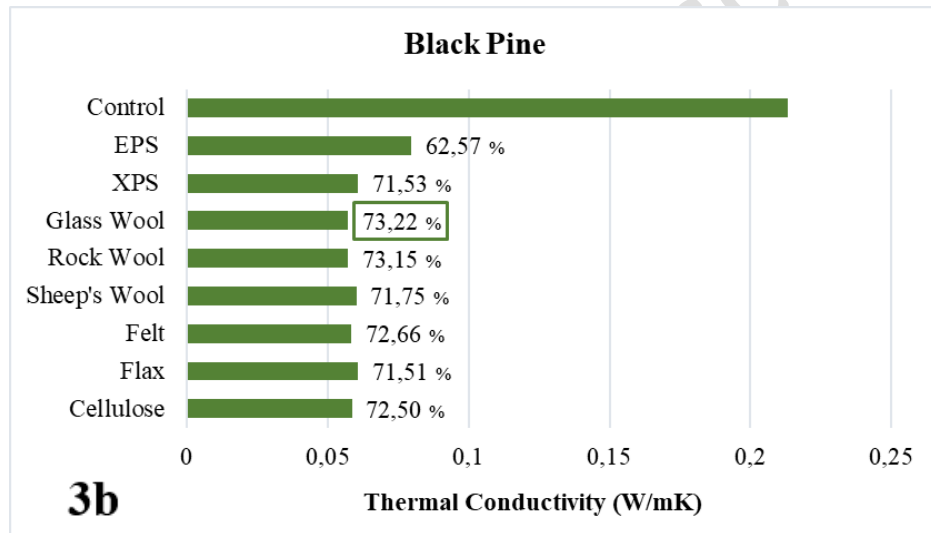
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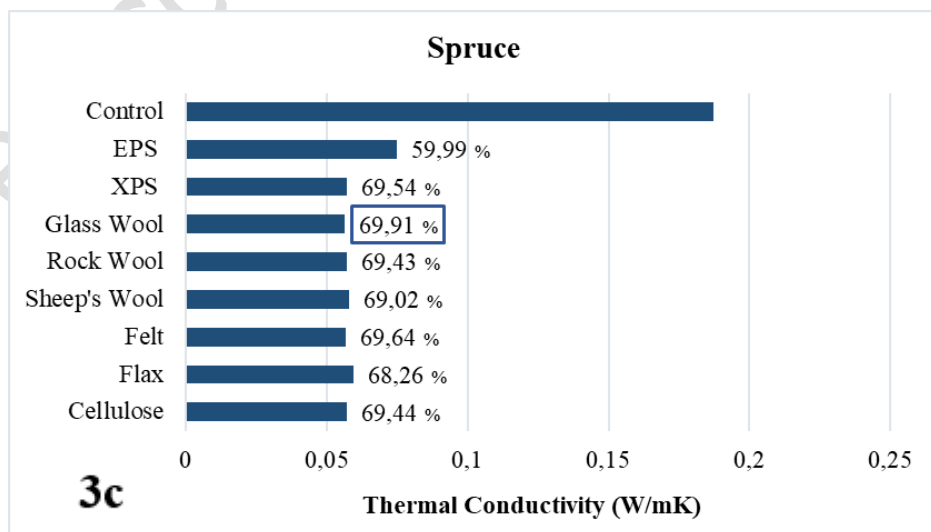
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**Figure 3:** Thermal conductivity values changes of the shear wall groups (3a; Scots pine, 3b; Black pine, 3c; Spruce).

277 In the comparison of the control groups with each other, it was determined that the  
278 highest thermal conductivity value was obtained from the shear walls formed with black  
279 pine plywood. The lowest value was found in the control group of shear walls formed  
280 with spruce plywood. It was stated in the literature that the most important factors on the  
281 thermal conductivity values of solid wood and wood-based panels were density and  
282 moisture content (Sonderegger 2011). Sonderegger and Niemz (2009) determined that  
283 the thermal conductivity of wood materials increased as the density and moisture content  
284 increased. In Table 2, the density and EMC of the veneer sheets and plywood panels used  
285 in the control groups of shear walls were given. It was observed that both density and  
286 EMC values of larch veneer and plywood were higher than the other two wood species.  
287 Likewise, the lowest of these values were obtained from spruce wood species. In addition,  
288 it could be seen from Table 2 and Table 4 that there was a linear relationship between the  
289 thermal conductivity values of the veneers and plywood and the values of the control  
290 groups of shear walls. Therefore, it was an expected result that the thermal insulation  
291 properties of spruce shear walls were better among the control groups.

292 When the data in Table 4 and the graphs in Figure 3 are examined, the thermal  
293 conductivity coefficient values of the black pine and spruce plywood shear walls  
294 produced with glass wool were found to be the lowest in percentage compared to the  
295 control groups. The lowest thermal conductivity coefficient was obtained from rock wool  
296 in the scots pine plywood shear walls. The reason for these results could be shown that  
297 the thermal conductivity coefficient values of glass and rock wool (0,038 W/mK and  
298 0,038 W/mK) were the lowest compared to other the thermal insulation materials (Table  
299 1). Ducoulombier and Lafhaj (2017) compared hygrothermal properties of glass wool,  
300 rock wool, EPS, wood fibreboard and polyester fibrefill and found similarly that the

301 thermal conductivity values of glass wool were the lowest. Domínguez-Muñoz *et al.*  
302 (2010) investigated that thermal conductivity of inorganic (cellular glass, glass and rock  
303 wool), organic (XPS, EPS, Polyurethane foam) and natural (sheep, cellulose and cotton)  
304 insulation materials. They observed that the inorganic materials have the lowest thermal  
305 conductivity values while the highest values were obtained from the organic materials. In  
306 this study, it was seen that similar results with the literature were obtained.

307 The percentage reduction in the thermal conductivity coefficient values was the  
308 least for all three species of wood in the shear wall groups produced with EPS panels. It  
309 was determined that the thermal conductivity of EPS foam (0,052 W/mK) was the highest  
310 among the thermal insulation materials (Table 1). Therefore, it was expected that the  
311 thermal conductivity values of plywood shear walls produced with EPS were also high.  
312 The glass wool is more porous material and have larger cavities than polystyrene  
313 materials (Berge and Johansson 2012). Heat flow occurs through the air in the cavities of  
314 the solids and the thermal conductivity of the air in the cavity is much lower than that of  
315 the solid material. This situation causes the whole material to have lower thermal  
316 conductivity (Zhou *et al.* 2010). Therefore, it was thought the plywood shear walls  
317 produced with glass wool gave the lowest thermal conductivity values according to  
318 polystyrene materials. Liu *et al.* (2020) determined the thermal conductivity of the  
319 wooden-frame walls that they formed with XPS and EPS in different configurations and  
320 observed that the thermal conductivity of the walls using EPS foam boards were higher  
321 than that of XPS. In order for an envelope of building to be considered as an insulating  
322 layer, it must have a thermal conductivity lower than 0,065 (W/mK) (Florea and Manea  
323 2019). According to the thermal conductivity results obtained from the study, the shear

324 wall groups except EPS can be used as an insulation layer in light-frame wooden  
325 buildings.

326 According to the percent difference values between the heat flux measured by the  
327 upper and lower HFM, EPS foam boards gave the lowest values among the thermal  
328 insulation materials for all of wood species. Hassanin *et al.* (2018) found that that the  
329 lowest percent difference values were obtained from the materials giving the highest  
330 thermal conductivity. A similar relationship was observed in this study. In the thermal  
331 conductivity coefficient measurements of the shear wall groups, the frames made of  
332 spruce timbers with similar density, moisture content and thermal conductivity values  
333 were used. In this way, the differences arising from the frame elements in the comparison  
334 of the thermal conductivity of the groups were minimized. Moreover, the metering area  
335 in the device was 100 mm x 100 mm as can be seen in Figure 2. The frame element was  
336 not included in the thermal conductivity metering area. The differences in the groups  
337 measured at the same temperature and relative humidity were entirely due to the plywood  
338 and thermal insulation material properties. The thermal conductivity values rather than  
339 density values of thermal insulation materials produced from materials with different  
340 properties (Table 1) showed a close relationship with the values of the shear wall groups.  
341 Similar thermal insulation materials used in all groups were the same properties.

342 In this study, after determining the thermal conductivity coefficient values of the  
343 shear wall groups, the absolute thermal resistance, thermal resistance, thermal resistivity  
344 and thermal conductance which are the most important parameters showing the thermal  
345 performance of the materials, were calculated and the results were given in Table 5.

346

347



**Table 5:** Thermal performance parameters of the shear wall groups.

Wall Numbers	Wood Species	Thermal Insulation Material Types	Absolute Thermal Resistance (R - K/W)	Thermal Resistance (R-value- m <sup>2</sup> K/W)	Thermal Resistivity (r-Km/W)	Thermal Conductance (C-W/m <sup>2</sup> K)
1	Scots Pine	Cellulose	99,365	0,994	16,810	1,006
2		Flax	100,878	1,009	17,013	0,991
3		Felt	103,136	1,031	17,431	0,970
4		Sheep's Wool	103,736	1,037	17,446	0,964
5		Rock Wool	107,496	1,075	18,142	0,930
6		Glass Wool	105,629	1,056	17,854	0,947
7		XPS	102,358	1,024	17,301	0,977
8		EPS	77,583	0,776	13,123	1,289
9		Control	29,550	0,295	5,000	3,384
10	Black Pine	Cellulose	103,420	1,034	17,065	0,967
11		Flax	99,931	0,999	16,472	1,001
12		Felt	104,039	1,040	17,161	0,961
13		Sheep's Wool	101,115	1,011	16,611	0,989
14		Rock Wool	106,089	1,061	17,479	0,943
15		Glass Wool	106,290	1,063	17,525	0,941
16		XPS	99,944	0,999	16,483	1,001
17		EPS	75,920	0,759	12,538	1,317
18		Control	28,442	0,284	4,693	3,516
19	Spruce	Cellulose	103,089	1,031	17,473	0,970
20		Flax	99,416	0,994	16,824	1,006
21		Felt	103,775	1,038	17,584	0,964
22		Sheep's Wool	102,062	1,021	17,232	0,980
23		Rock Wool	103,397	1,034	17,467	0,967
24		Glass Wool	104,692	1,047	17,743	0,955
25		XPS	103,419	1,034	17,525	0,967
26		EPS	78,661	0,787	13,346	1,271
27		Control	31,475	0,315	5,339	3,177

349

350 The changes in thermal resistance values of the shear wall groups whose thermal  
 351 conductivity coefficient values were determined experimentally were found similarly. Liu  
 352 *et al.* (2018) measured the thermal resistance of the wooden-frame walls that they formed

353 with glass wool, XPS and EPS in different configurations and found that EPS foam boards  
354 have the lowest thermal resistance values while the lowest values were obtained from  
355 glass wool. The other thermal performance parameters also varied in parallel with both  
356 thermal resistance and thermal conductivity coefficient values. Kumar *et al.* (2020)  
357 compared the properties and thermal performances of some building insulation materials  
358 and determined thermal conductivity coefficient value ranges for these materials. These  
359 ranges were 0,037 W/mK - 0,042 W/mK for cellulose, 0,033 W/mK - 0,090 W/mK for  
360 flax, 0,030 W/mK - 0,054 W/mK for sheeps's wool, 0,033 W/mK - 0,040 W/mK for rock  
361 wool and 0,030 W/mK - 0,050 W/mK for glass wool. Similarly, Wang *et al.* (2018) found  
362 that the thermal conductivity of rock wool ranges from 0,035 W/mK to 0,039 W/mK. In  
363 this study, it was determined that the measured thermal conductivity values of the thermal  
364 insulation materials were between these ranges. Moreover, the density values of all the  
365 materials used in the study except EPS were among the value ranges determined in the  
366 literature (Kumar *et al.* 2020; Anh and Pásztor 2021). According to FAO (2022), EPS  
367 densities vary between 10 kg/m<sup>3</sup> and 33 kg/m<sup>3</sup>, and the thermal conductivity value of EPS  
368 foam with a density of 10 kg/m<sup>3</sup> is 0,057 W/mK. Dujive (2012) found the thermal  
369 resistance of rock wool and glass wool used as wall insulation material from 1 m<sup>2</sup>K/W to  
370 1,5 m<sup>2</sup>K/W and also found the thermal resistance of the empty cavity wall as 0,35 m<sup>2</sup>K/W.  
371 These thermal resistance values were found to be close to the values found in the study.  
372 However, the results of the study could not be compared with the literature due to the  
373 absence of studies in which plywood sheathed shear walls were filled with thermal  
374 insulation materials.

375

376

## CONCLUSIONS

377

378 In this study, thermal performances of plywood shear walls, where thermal  
379 insulation is extremely important in light-frame wooden buildings, were compared  
380 according to the type of insulation materials used. In determining the thermal  
381 performances, different parameters such as thermal conductivity coefficients and thermal  
382 resistance values were used. When the measured thermal conductivity values and other  
383 calculated thermal parameters are examined, the shear walls produced with EPS foam  
384 boards have been identified as the groups with the worst thermal performance. Rock wool  
385 was the best thermal insulation material among the scots pine shear wall groups while  
386 glass wool was the best thermal insulation material among the black pine and spruce shear  
387 wall groups. The shear walls produced with spruce plywood indicated better thermal  
388 performance than other wood species. The thermal conductivity values obtained as a  
389 result of the study remained below the value of 0,065 W/mK, excluding EPS foam board.  
390 This case proved the shear wall groups formed in this study can be used for thermal  
391 insulation in light-frame wooden buildings.

392

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